



Standard Test Method for Instrumented Impact Testing of Metallic Materials¹

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1. Scope

1.1 This test method establishes the requirements for performing instrumented Charpy V-Notch (CVN) and instrumented Miniaturized Charpy V-Notch (MCVN) impact tests on metallic materials. This method, which is based on experience developed testing steels, provides further information (in addition to the total absorbed energy) on the fracture behavior of the tested materials. Minimum requirements are given for measurement and recording equipment such that similar sensitivity and comparable total absorbed energy measurements to those obtained in Test Methods E23 and E2248 are achieved.

1.2 The values stated in SI units are to be regarded as standard. No other units of measurement are included in this standard.

1.3 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.*

2. Referenced Documents

2.1 ASTM Standards:²

A370 Test Methods and Definitions for Mechanical Testing of Steel Products

E4 Practices for Force Verification of Testing Machines

E23 Test Methods for Notched Bar Impact Testing of Metallic Materials

E177 Practice for Use of the Terms Precision and Bias in ASTM Test Methods

E691 Practice for Conducting an Interlaboratory Study to Determine the Precision of a Test Method

E2248 Test Method for Impact Testing of Miniaturized Charpy V-Notch Specimens

¹ This test method is under the jurisdiction of ASTM Committee E28 on Mechanical Testing and is the direct responsibility of Subcommittee E28.07 on Impact Testing.

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² For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

2.2 ISO Standard:

ISO 14556 Steel—Charpy V-notch Pendulum Impact Tests—Instrumented Test Method³

3. Terminology

3.1 *Definitions*—The symbols and definitions applicable to instrumented impact testing are indicated in Table 1.

4. Summary of Test Method

4.1 This test method prescribes the requirements for instrumented CVN and MCVN impact tests in accordance with Test Methods E23 and E2248. The E23 and E2248 tests consist of breaking by one blow from a swinging pendulum, under conditions defined hereafter, a specimen notched in the middle and supported at each end. In order to establish the impact force-displacement diagram, it is necessary to instrument the striker with strain gages⁴ and measure the voltage as a function of time during the impact event. The voltage-time curve is converted to the force-time curve through a suitable static calibration. The force-displacement relationship is then obtained by double integration of the force-time curve. The area under the force-displacement curve corresponds to the energy absorbed by the specimen during the test.

4.2 Force-displacement curves for different steels and different temperatures can vary even though the areas under the curves and the absorbed energies are identical. If the force-displacement curves are divided into a number of characteristic parts, various phases of the test with characteristic forces, displacements, and energies can be deduced. These characteristic values provide additional information about the fracture behavior of the specimen.

4.3 Application of instrumented test data to the evaluation of material behavior is the responsibility of the user of this test method.

5. Significance and Use

5.1 Instrumented impact testing provides an independent measurement of the total absorbed energy associated with

³ Available from American National Standards Institute (ANSI), 25 W. 43rd St., 4th Floor, New York, NY 10036, <http://www.ansi.org>.

⁴ This test method refers to strikers instrumented with strain gages. However, the use of piezoelectric load cells or accelerometers is not excluded, provided their temperature sensitivity is properly accounted for.

TABLE 1 Symbols and Designations Related to Instrumented Impact Testing

Symbol	Definition	Unit
F_a	Force at end of unstable crack propagation (arrest force)	N
F_{gy}	General yield force	N
F_m	Maximum force	N
F_{bf}	Force at initiation of brittle fracture (unstable crack propagation)	N
g	Local acceleration due to gravity	m/s ²
h_0	Initial falling height of the striker	m
KV	Absorbed energy measured from the machine dial or encoder	J
m	Total effective mass of moving striker	kg
s_a	Displacement at end of unstable crack propagation (arrest force)	m
s_{gy}	Displacement at general yield	m
s_m	Displacement at maximum force	m
s_{bf}	Displacement at initiation of brittle fracture	m
s_t	Displacement at end of force-displacement curve	m
t_0	Time at the beginning of deformation of the specimen	s
v_0	Initial striker impact velocity	ms ⁻¹
W_a	Partial impact energy from $F = 0$ to $F = F_a$	J
W_{bf}	Partial impact energy from $F = 0$ to $F = F_{bf}$	J
W_m	Partial impact energy from $F = 0$ to $F = F_m$	J
W_t	Total impact energy	J

fracturing CVN or MCVN specimens for test machines equipped with a dial and/or optical encoder.

5.2 Instrumented impact testing is particularly effective in MCVN testing since the resolution of a calibrated strain-gaged striker does not necessarily decrease with the magnitude of the measured energy.

5.3 In addition to providing an measure of total absorbed energy (W_t), instrumented testing enables the determination of characteristic force, energy, and displacement parameters. Depending on the material and test temperature, these parameters can provide very useful information (in addition to total absorbed energy) on the fracture behavior of materials such as: the temperature which corresponds to the onset of the lower shelf; the temperature which corresponds to the onset of the upper shelf; the pre-maximum force energy (W_m); the post-maximum force energy; the energy associated with shear lip tearing after brittle fracture; the general yield force (F_{gy}); the force at brittle fracture initiation (F_{bf}); the arrest force (F_a). The instrumented data may also be used to highlight test results which should be discarded on the basis of misalignment or other critical test factors.

6. Precautions in Operation of the Machine

6.1 Safety precautions should be taken to protect personnel from electric shock, the swinging pendulum, flying broken specimens, and hazards associated with specimen warming and cooling media. See also 1.3.

7. Apparatus

7.1 The test shall be carried out in accordance with Test Methods E23 or E2248 using a pendulum impact testing machine which is instrumented to determine force-time or force-displacement curves.

7.1.1 For instrumented CVN testing, the use of an instrumented striker conforming to the specifications of ISO 14556

(i.e., 2 mm radius of striking edge) is allowed. Available data (1, 2)⁵ indicate that the influence of striker geometry on instrumented CVN forces is not very significant.

7.2 Force Measurement:

7.2.1 Force measurement is achieved by using an electronic sensor (piezoelectric load cell, strain gage load cell or a force measurement derived from an accelerometer).

7.2.2 The force measuring system (including strain gages, wiring, and amplifier) shall have an upper frequency bound of at least 100 kHz for CVN tests and 250 kHz for MCVN tests. For MCVN tests, if only absorbed energy has to be measured from the curve, an upper frequency limit of 100 kHz is sufficient. The upper frequency bound for the system shall be verified by measurement or analysis. Measurements can be made using a function generator which is wired directly to the strain gage bridge.

7.2.3 The signal shall be recorded without filtering. Post-test filtering, however, is allowed.

7.2.4 Calibration of the recorder and measurement system may be performed statically in accordance with the accuracy requirements given below. It is recommended that the force calibration be performed with the striker attached to the pendulum assembly. The strain gage signal conditioning equipment, cables, and recording device shall be used in the calibration. In most cases, a computer is used for data acquisition and the calibration shall be performed with the voltage read from the computer. The intent is to calibrate through the electronics and cables which are used during actual testing. Force is applied to the striker by using a suitable load frame with a load cell verified in accordance with Practices E4.

7.2.4.1 The static linearity and hysteresis error of the built-in, instrumented striker, including all parts of the measurement system up to the recording apparatus (printer, plotter, etc.), shall be within $\pm 2\%$ of the recorded force, between 50 and 100 % of the nominal force range, and within $\pm 1\%$ of the full scale force value between 10 and 50 % of the nominal force range (see Fig. 1).

7.2.4.2 The instrumented striker system shall be calibrated to ensure accurate force readings are obtained over the nominal force range which will be encountered in testing. The strain gaged system shall be designed to minimize its sensitivity to non-symmetric loading.

7.2.5 Calibration shall be performed if the instrumented striker has undergone dismantling or repair, unless it can be shown that removal of the striker from the test machine, and subsequent reattachment to the machine, does not affect the calibration. Calibration shall also be performed under the circumstances described below.

7.2.6 *Requirements on Absorbed Energy*—For each test in which the entire force signal has been recorded (i.e., until the force returns to the baseline), the difference between absorbed energy given by the dial and/or optical encoder KV and the total impact energy W_t shall be within 15 % or 1 J, whichever is larger. If this requirement is not met but the difference does not exceed 25 % or 2 J, whichever is larger, force values shall

⁵ The boldface numbers in parentheses refer to the list of references at the end of this standard.

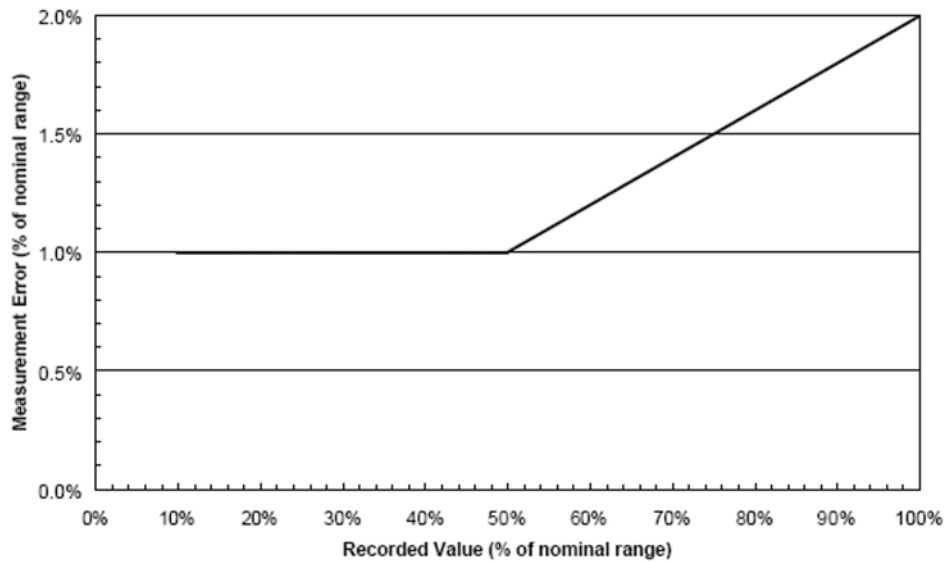


FIG. 1 Allowable Errors in Force Measurements

be adjusted until $KV = W_t$ within 0.01 J (3). If the difference exceeds 25 % or 2 J, whichever is larger, the test shall be discarded and the user shall check and if necessary repeat the calibration of the instrumented striker. If recording of the entire force signal is not possible (for example due to the specimen being ejected from the machine without being fully broken), the user shall demonstrate conformance to the requirements above by testing at least five Charpy specimens of any equivalent material.

NOTE 1—Specimens with certified values of maximum force (F_m) can be tested to verify the accuracy of the force values measured by the instrumented striker. Dynamic impact force verification specimens are available⁶ with certified F_m values of 24.06 kN and 33.00 kN. These values have been established at room temperature through an interlaboratory study (4) involving six international laboratories, see also 13.1.3. The same verification specimens can also be used to verify the absorbed energy scale of the impact machine in accordance with Test Methods E23 at either $-40\text{ }^{\circ}\text{C} \pm 1\text{ }^{\circ}\text{C}$ or room temperature ($21\text{ }^{\circ}\text{C} \pm 1\text{ }^{\circ}\text{C}$).

7.3 Displacement Determination:

7.3.1 Displacement is normally determined by converting a strain gage voltage-time measurement to a force-time measurement. The force-time relationship is proportional to the acceleration as a function of time. Given an assumed rigid striker of mass m , the initial impact velocity v_0 , the time t following the beginning of the deformation at t_0 , and expressing the velocity as a function of time by $v(t)$, the specimen bending displacement $s(t)$ is calculated by double numerical integration as follows:

$$v(t) = v_0 - \frac{1}{m} \int_{t_0}^t F(t) dt \quad (1)$$

$$s(t) = \int_{t_0}^t v(t) dt \quad (2)$$

7.3.2 The initial impact velocity needed to perform the above integrations may be calculated from:

$$v_0 = \sqrt{2gh_0} \quad (3)$$

where:

g = the local acceleration due to gravity, and
 h_0 = the falling height of the striker.

7.3.2.1 Alternatively, the velocity signal registered when the pendulum passes through its lowest position and strikes the specimen can be optically measured directly to determine v_0 .

7.3.3 Displacement can also be determined by non-contacting measurement of the displacement of the striker relative to the anvil using optical, inductive, or capacitive methods. The signal transfer characteristics of the displacement measurement system must correspond to that of the force measuring system in order to make the two recordings synchronous. The displacement measuring system shall be designed for nominal values of up to 30 mm. Linearity errors in the measuring system shall yield measured values to within +2 % in the range 1–30 mm. Measurements between zero and 1 mm may not be sufficiently accurate to determine the displacement. In such cases, it is recommended that the displacement of the specimen be determined from time measurement and the striker impact velocity as indicated in Eq 1 and 2.

7.4 Recording Apparatus:

7.4.1 The minimum data acquisition requirement is a 10-bit analog-digital converter with a minimum sampling rate of 1000 data points per millisecond. However, 12-bit or more is recommended. A minimum storage capacity of 8000 data points is required.

7.4.2 The total absorbed energy measured using instrumentation shall be compared with that shown by the machine dial (only for CVN testing), or preferably, by comparison with an optical encoder (for both CVN and MCVN testing). If total absorbed energy is measured using a machine dial or optical

⁶ If interested, email charpy@boulder.nist.gov.

encoder, then this data shall be reported along with the instrumented striker energy. For requirements on absorbed energy based on the comparison between KV and W_p , refer to 7.2.6.

8. Test Specimens

8.1 The CVN specimens shall be in accordance with Test Method E23. The MCVN specimens shall be in accordance with Test Method E2248.

9. Procedure

9.1 *Specimen Testing*—The test is performed in the same way as the CVN or MCVN impact test according to Test Methods E23 or E2248, respectively. In addition, the voltage-time curve is measured and evaluated to give the force-displacement curve. The force-displacement curve is evaluated with respect to the characteristic phases of the deformation and fracture stages.

9.2 *Data Acquisition*—The high speed acquisition system (the portion of the system which is capable of storing the dynamic response signal) shall be triggered such that baseline data before loading and after fracture (or release of the specimen from the anvils) is retained in computer memory.

10. Characteristics of the Force-Displacement Curve

10.1 *Type of Force-Displacement Curve*—Representative force-displacement curves and their characteristic force values are illustrated in Fig. 2.

10.2 Characteristic Values of Force:

10.2.1 The general yield force F_{gy} is the force at the transition point from the initial linear elastic part, discarding the inertia peaks (normally one, unless the specimen was not fully in contact with the anvils), to the curved increasing part of the force-displacement curve. It serves, to a first approximation, as an indication of yielding across the entire ligament.

10.2.2 The maximum force F_m corresponds to the maximum value of the curve fitted through the oscillations of the force-displacement curve following the onset of yield of the entire ligament.

10.2.3 The force at the initiation of unstable crack propagation F_{bf} is the force at the beginning of the steep drop in the force-displacement curve. It characterizes the beginning of unstable crack propagation.

10.2.4 The force at the end (arrest) of unstable crack propagation is F_a .

10.3 *Characteristic Values of Displacement*—The forces defined in 10.2 have corresponding displacements which are given the same subscripts as the forces. In addition, a displacement corresponding to the end of the force-displacement curve, s_p , is defined.

10.3.1 The displacement at the onset of general yielding of the ligament is s_{gy} .

10.3.2 The displacement at maximum force is s_m .

10.3.3 The displacement at the initiation of unstable crack propagation is s_{bf} .

10.3.4 The displacement at the end (arrest) of unstable crack propagation is s_a (generally, s_a is approximately equal to s_{bf} due to the steep drop in the force-displacement curve between F_{bf} and F_a).

10.3.5 The displacement at the end of the force-displacement curve is s_p . This point is defined as the displacement at which the force has decreased to the pre-test baseline value.

10.4 Characteristic Values of Impact Energy:

10.4.1 Given the force definitions in 10.1, the force-displacement curve may be partitioned and corresponding energies may be determined. The values of the partial impact energies are given the same subscript as the force at the end of the appropriate part of the force-displacement curve.

10.4.2 The area under the complete force-displacement curve up to s_p is the total impact energy with the abbreviation W_p .

10.4.3 The impact energy up to maximum force is W_m .

10.4.4 The impact energy up to the force at the initiation of unstable crack propagation is W_{bf} .

10.4.5 The impact energy up to the force at the arrest of unstable crack propagation is W_a (on account of the steep drop in the force-displacement curve between F_{bf} and F_a , it is generally the case that W_{bf} is approximately equal to W_a).

11. Evaluation of the Force-Displacement Curve

11.1 The force-displacement curve is determined by double numerical integration of the force-time curve.

11.2 Representative force-displacement curves of various types are given in Fig. 2. These can be grouped as the following types:

Type A	Lower shelf (brittle fracture)
Type B	Ductile-to-Brittle Transition Region (mixed mode fracture)
Type C	Upper shelf (ductile fracture)

NOTE 2—The type of force-displacement curve may be determined by comparison with the examples shown in Fig. 2.

11.2.1 With force-displacement curves of type A, typically only unstable (brittle) crack propagation occurs. For type B, various amounts of stable and unstable crack propagation can occur. For type C, only stable (ductile) crack propagation occurs.

11.3 A condition for further evaluation of the force-displacement curve is the occurrence of a well defined general yield force F_{gy} . It should be noted that force oscillations are observed on the pre-maximum force test record which arise from force interaction between the striker and the specimen. These oscillations are usually damped out by plasticity before maximum force.

11.4 Determination of the Characteristic Values of Force:

11.4.1 The force F_{gy} is defined as the force at the intersection of the linear elastic part of the force-displacement curve, discarding inertia peak(s), and the fitted curve through the oscillations of the force-displacement curve following the onset of general yielding of the uncracked ligament.

11.4.2 The force F_m is determined as the maximum value of the fitted data in the region of maximum force, after the

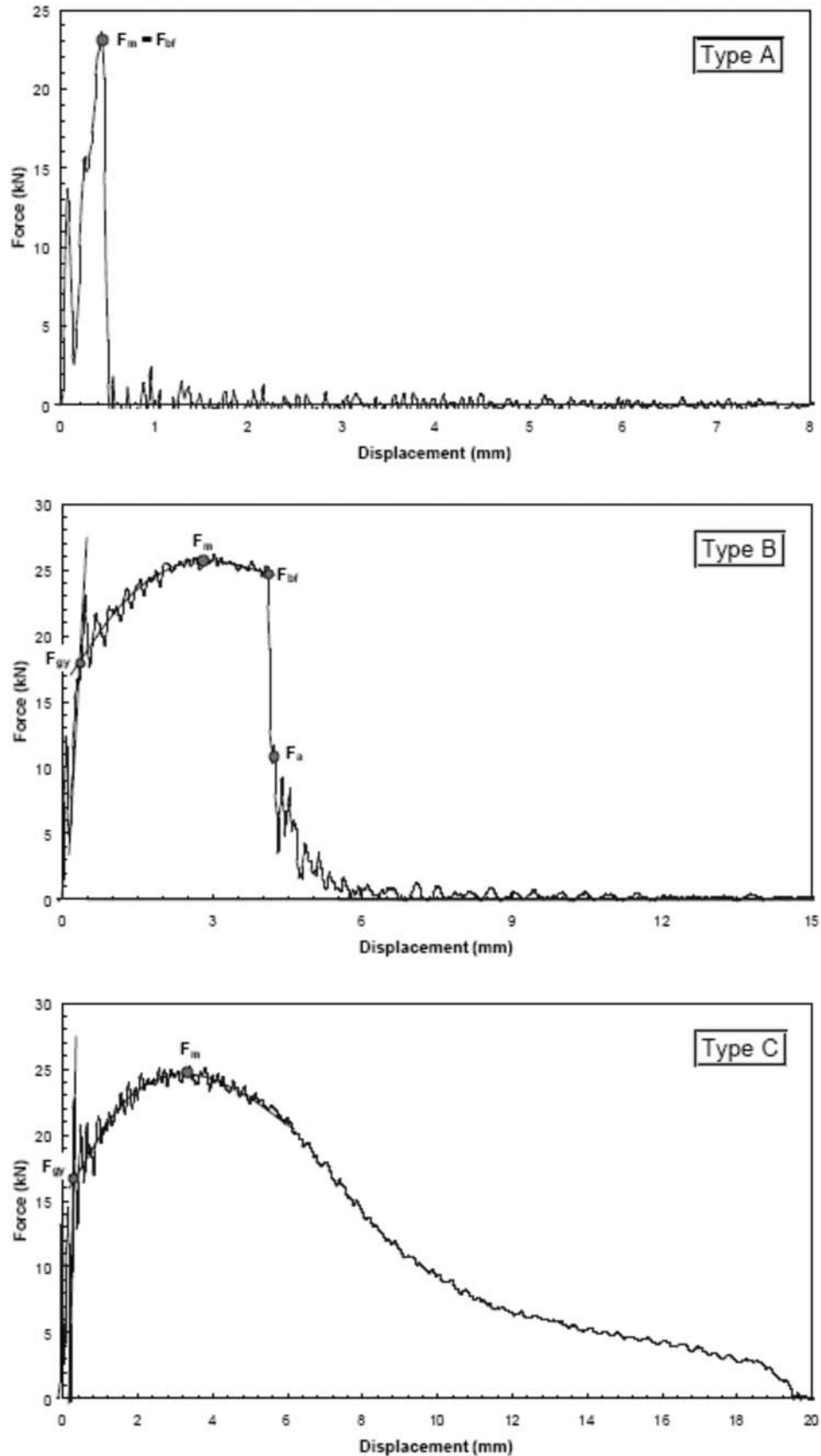


FIG. 2 Characteristic Force-Displacement Curves and Definitions of Characteristic Forces

occurrence of general yield. In cases where fracture occurs early in the force-displacement curve prior to general yield force (Type A), the maximum force is defined as the force at which the rapid force drop begins.

11.4.3 The force F_{bf} is determined as the force at the intersection of the fitted curve through the oscillations and the steeply dropping part of the force-displacement curve. If the steep drop coincides with the maximum recorded force, then $F_{bf} = F_m$ (force-displacement curve of type A).

11.4.4 The force F_a is determined as the force at the intersection of the steep drop of the force-displacement curve and the fitted curve through the oscillations of the subsequent part of the force-displacement curve (force-displacement curves of type B). If the unstable crack is not arrested, $F_a = 0$.

11.5 Determination of the Characteristic Values of Displacement:

11.5.1 The characteristic values of displacement are the abscissa values of the characteristic values of force determined in accordance with 11.4.

11.5.2 The displacement s_i is determined by comparing the force to the original baseline signal and defining the end of the test as the displacement which corresponds to the force returning within the scatter of the pre-test baseline signal.

11.6 Determination of the Characteristic Values of Impact Energy—The characteristic values of impact energy are determined by numerical integration of the appropriate parts of the force-displacement curve.

11.7 Determination of the Percent Shear Area on the Fracture Surface—Test Method E23 provides a description of several methods for measuring the percentage of shear fracture area on the test specimen fracture surface. While these measurements can be made for many steels, there are cases where this measurement is difficult because the brittle and ductile fracture areas are hard to resolve optically. An alternative approach is to use the instrumented impact data to calculate the percent shear area. If, in the course of the force-displacement curve, there is no steep drop of force occurring (curves of type C in Fig. 2), this may indicate that the ductile proportion of the fracture surface amounts to 100 % of the total fracture surface. If a steep drop of force occurs, the amount of the drop in relation to other characteristic force values allows an approximate value of the proportion of ductile fracture surface (% shear) to be calculated. Several researchers have reported good correlation for pressure vessel materials using one or more of the equations given below (1, 5):

$$\% \text{ shear} = \left[1 - \frac{F_{bf} - F_a}{F_m} \right] \times 100 \quad (4)$$

$$\% \text{ shear} = \left[1 - \frac{F_{bf} - F_a}{F_m + (F_m - F_{gy})} \right] \times 100 \quad (5)$$

$$\% \text{ shear} = \left[1 - \frac{F_{bf} - F_a}{F_m + k(F_m - F_{gy})} \right] \times 100 \quad \text{with } k \approx 0.5 \quad (6)$$

$$\% \text{ shear} = \left[1 - \sqrt{\frac{\frac{F_{gy}}{F_m} + 2}{3}} \times \left(\sqrt{\frac{F_{bf}}{F_m}} - \sqrt{\frac{F_a}{F_m}} \right) \right] \times 100 \quad (7)$$

$$\% \text{ shear} = \left[1 - \frac{F_{bf} - F_a}{0.5(F_{gy} + F_m)} \right] \times 100 \quad (8)$$

11.7.1 These equations do not all characterize steel behavior well and comparisons should be made with physical measurements. The acceptable methods for physical measurement of percent shear fracture area are given in Test Method E23. Errors of the order of 20 % have been observed for some materials.

12. Report

12.1 The minimum reporting requirements given in Test Methods E23 or E2248 shall be satisfied.

12.2 Test equipment characteristics, including: response frequency of the system; number of data points acquired; number of data points acquired per millisecond; and any adjustments made to the integrated total absorbed energy to achieve agreement with the dial or encoder absorbed energy.

12.3 Total energy absorbed, as recorded by the machine dial and/or encoder.

12.4 Type of force-displacement curve (A, B or C) and illustration of the force-displacement curve.

12.5 Characteristic values of force, displacement and impact energy.

13. Precision and Bias

13.1 Precision—Instrumented impact data from five interlaboratory studies have been analyzed in accordance with Practice E691 in order to establish the precision of this Test Method. The terms repeatability limit and reproducibility limit are used as specified in Practice E177.

13.1.1 CVN Specimens—Results from three interlaboratory studies are used to establish the precision of this Test Method for CVN specimens.

13.1.2 An interlaboratory study (6) of characteristic instrumented impact forces, displacements and energies was conducted using Charpy V-notch specimens (E23 Type A) of A533B C1.1 (tested at room temperature and 150°C) and two reference materials produced by the National Institute of Standards and Technology, Boulder CO (low energy and high energy). The ILS was conducted in accordance with Practice E691 in eight laboratories, each one obtaining from five to six test results for each test parameter (Table 2). See ASTM Research Report No. E28–1040.⁷

13.1.3 Another interlaboratory study (2) of characteristic instrumented impact forces and energies was conducted using Charpy V-notch specimens (E23 Type A) of two reference materials produced by the National Institute of Standards and Technology, Boulder CO (low energy and high energy). The ILS was conducted in accordance with Practice E691 in six laboratories with eight different test machines providing ten test results for each test parameter (Table 3). See ASTM Research Report No. E28–1035.⁸

13.1.4 A third interlaboratory study (7) of characteristic instrumented impact forces and energies was conducted using

⁷ Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report RR:E28-1040.

⁸ Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report RR:E28-1035.

TABLE 2 Results from ILS on CVN specimens (6)

Parameter	Material	Average	Repeatability Standard Deviation	Reproducibility Standard Deviation	Repeatability Limit	Reproducibility Limit
F_{gy} , kN	A553B (RT)	13.03	0.82	1.39	2.29	3.88
	A533B (150°C)	11.10	0.44	1.08	1.22	3.01
	4340 (low en)	33.48	1.00	2.90	2.81	8.13
	4340 (high en)	19.95	0.67	1.87	1.89	5.25
F_m , kN	A553B (RT)	18.71	0.35	0.75	0.98	2.11
	A533B (150°C)	16.88	0.34	0.69	0.94	1.94
	4340 (low en)	34.22	0.70	1.70	1.95	4.77
	4340 (high en)	24.80	0.23	0.61	0.64	1.71
F_{bf} , kN	A553B (RT)	17.83	0.78	1.14	2.18	3.18
	4340 (low en)	33.09	1.40	2.75	3.91	7.70
F_a , kN	A553B (RT)	7.37	1.43	2.88	4.01	8.07
	4340 (low en)	1.08	0.88	1.99	2.47	5.56
s_m , mm	A553B (RT)	3.03	0.21	0.33	0.58	0.92
	A533B (150°C)	3.45	0.23	0.29	0.66	0.82
	4340 (low en)	0.88	0.03	0.07	0.09	0.20
	4340 (high en)	1.78	0.12	0.31	0.34	0.88
W_b , J	A553B (RT)	77.61	18.12	18.12	50.73	50.73
	A533B (150°C)	130.75	5.67	5.79	15.87	16.22
	4340 (low en)	23.91	1.84	2.63	5.16	7.36
	4340 (high en)	119.01	6.37	7.10	17.84	19.89

TABLE 3 Results from ILS on CVN specimens (2)

Parameter	Energy Level	Average	Repeatability Standard Deviation	Reproducibility Standard Deviation	Repeatability Limit	Reproducibility Limit
F_{gy} , kN	Low	29.85	0.68	4.19	1.89	11.73
	High	19.42	0.40	1.09	1.12	3.06
F_m , kN	Low	31.90	0.65	3.85	1.82	10.79
	High	23.50	0.16	1.96	0.44	5.49
W_b , J	Low	18.63	0.63	1.23	1.76	3.45
	High	108.39	2.55	4.13	7.13	11.55

TABLE 4 Results from ILS on CVN specimens (7)

Parameter	Average	Repeatability Standard Deviation	Reproducibility Standard Deviation	Repeatability Limit	Reproducibility Limit
F_{gy} , kN	18.42	0.38	1.24	1.06	3.46
F_m , kN	23.97	0.07	1.85	0.20	5.19
W_b , J	146.69	3.73	11.34	10.43	31.74

Charpy V-notch specimens (E23 Type A) of one reference material produced by the Institute for Reference Materials and Measurements, Geel Belgium (ERM high energy). The ILS was conducted in accordance with Practice E691 in nine laboratories, each providing two test results for each test parameter (Table 4). See ASTM Research Report No. E28-1036.⁹

13.1.5 *MCVN Specimens*—Results from two interlaboratory studies are used to establish the precision of this Test Method for MCVN specimens.

13.1.6 An interlaboratory study (6) of characteristic instrumented impact forces, displacements and energies was conducted using miniaturized Charpy V-notch specimens with square cross section ($4.83 \times 4.83 \text{ mm}^2$) of A533B C1.1 (tested at room temperature and 150°C) and of two reference materials produced by the National Institute of Standards and Technology, Boulder CO (low energy and high energy). The

ILS was conducted in accordance with Practice E691 in six laboratories, each one obtaining up to six test results for each test parameter (Table 5). See ASTM Research Report No. E28-1038.¹⁰

13.1.7 Another interlaboratory study (8, 9) of characteristic instrumented impact forces, displacements and energies was conducted using miniaturized Charpy V-notch specimens with rectangular cross section ($3 \times 4 \text{ mm}^2$) of A533B C1.1. The ILS was conducted in accordance with Practice E691 in thirteen laboratories with fourteen test machines, each one obtaining up to five test results for each test parameter (Table 6). See ASTM Research Report No. E28-1037.¹¹

13.2 *Bias*—This Test Method has no bias because characteristic instrumented impact forces, displacement and energies are defined only in terms of this Test Method. Furthermore,

¹⁰ Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report RR:E28-1038.

¹¹ Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report RR:E28-1037.

⁹ Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report RR:E28-1036.

TABLE 5 Results from ILS on MCVN specimens (6)

Parameter	Material	Average	Repeatability Standard Deviation	Reproducibility Standard Deviation	Repeatability Limit	Reproducibility Limit
F_{gy} , kN	A553B (RT)	2.78	0.19	0.37	0.53	1.04
	A533B (150°C)	2.56	0.13	0.17	0.35	0.47
	4340 (low en)	4.58	0.11	0.63	0.30	1.77
	4340 (high en)	3.62	0.16	0.53	0.45	1.49
F_m , kN	A553B (RT)	3.76	0.06	0.26	0.17	0.72
	A533B (150°C)	3.25	0.06	0.37	0.17	1.03
	4340 (low en)	4.89	0.10	0.43	0.29	1.19
	4340 (high en)	4.64	0.08	0.61	0.23	1.72
s_m , mm	A553B (RT)	1.14	0.06	0.11	0.16	0.30
	A533B (150°C)	1.34	0.06	0.12	0.17	0.34
	4340 (low en)	0.76	0.05	0.07	0.15	0.18
	4340 (high en)	0.76	0.04	0.05	0.12	0.15
W_b , J	A553B (RT)	11.01	0.47	0.76	1.31	2.14
	A533B (150°C)	10.97	0.41	0.57	1.16	1.60
	4340 (low en)	10.75	0.36	0.91	1.02	2.54
	4340 (high en)	10.81	0.25	0.82	0.70	2.31

TABLE 6 Results from ILS on MCVN specimens (8, 9)

Parameter	Average	Repeatability Standard Deviation	Reproducibility Standard Deviation	Repeatability Limit	Reproducibility Limit
F_{gy} , kN	0.98	0.03	0.04	0.08	0.11
F_m , kN	1.31	0.02	0.05	0.06	0.13
s_{gy} , mm	0.18	0.02	0.04	0.06	0.12
s_m , mm	1.91	0.10	0.14	0.29	0.40
s_b , mm	11.79	0.23	1.36	0.65	3.79
W_m , J	2.21	0.16	0.22	0.46	0.61
W_b , J	8.35	0.42	0.71	1.18	1.99
KV , J	8.22	0.43	0.71	1.19	1.98

since there is no accepted reference material, method, or laboratory suitable for determining the bias for the procedure in this Test Method, no statement on bias is being made.

14. Keywords

14.1 fracture appearance; impact test; instrumented impact testing; miniaturized Charpy test; notched specimens; pendulum machine

REFERENCES

- (1) Nanstad, R. K., and Sokolov, M. A., “Charpy Impact Test Results on Five Materials and NIST Verification Specimens Using Instrumented 2-mm and 8-mm Strikers,” Pendulum Impact Machines: Procedures and Specimens for Verification, ASTM STP 1248, T. A. Siewert, and A. K. Schmieder, eds., ASTM, 1995, pp. 111-139.
- (2) McCowan, C. N., Splett, J. D., and Lucon, E., “Dynamic Force Measurement: Instrumented Charpy Impact Testing,” NISTIR 6652, January 2008 .
- (3) Lucon, E., Chaouadi, R., and van Walle, E., “Different Approaches for the Verification of Force Values Measured with Instrumented Charpy Strikers,” Pendulum Impact Machines: Procedures and Specimens, ASTM STP 1476, T. A. Siewert, M. P. Manahan, Sr., and C. N. McCowan, eds., ASTM, 2006, pp. 95-103.
- (4) McCowan, C. N., Santoyo, R. L., and Splett, J. D., “Certification Report for SRMs 2112 and 2113,” NIST Special Publication 260-172, July 2009.
- (5) van Walle, E., “Evaluating Material Properties by Dynamic Testing,” ESIS Publication 20, 1996 (European Structural Integrity Society), Mechanical Engineering Publications Limited, Northgate Avenue, Bury St. Edmunds, Suffolk, IP32 6BW UK, 1996.
- (6) Manahan, M. P., Sr., Martin F. J., and Stonesifer, R. B., “Results of the ASTM Instrumented/Miniaturized Round Robin Test Program,” Pendulum Impact Testing: A Century of Progress, ASTM STP 1380, T. A. Siewert and M. P. Manahan, Sr., Eds., American Society for Testing and Materials, West Conshohocken, PA, 1999.
- (7) International Atomic Energy Agency, Final Report of Coordinated Research Project 8 (CRP-8), “Master Curve Approach to Monitor Fracture Toughness of Reactor Pressure Vessels in Nuclear Power Plants,” in preparation.
- (8) Lucon, E., “Round-Robin on Instrumented Impact Testing of Sub Size Charpy-V Specimens: Results of Phase 1,” ESIS TC5, Final Report, 2 April 1998 .
- (9) Lucon, E., “European Activity on Instrumented Impact Testing of Subsize Charpy V-Notch Specimens (ESIS TC5),” Pendulum Impact Testing: A Century of Progress, ASTM STP 1380, T. A. Siewert, and M. P. Manahan, Sr., Eds., American Society for Testing and Materials,

West Conshohocken, PA, 1999, pp. 242-252.

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