



Standard Practice for Shearography of Polymer Matrix Composites, Sandwich Core Materials and Filament-Wound Pressure Vessels in Aerospace Applications¹

This standard is issued under the fixed designation E 2581; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (ε) indicates an editorial change since the last revision or reapproval.

1. Scope

1.1 This practice describes procedures for shearography of polymer matrix composites, sandwich core materials, and filament-wound pressure vessels made entirely or in part from fiber-reinforced polymer matrix composites. The composite materials under consideration typically contain continuous high modulus (greater than 20 GPa (3×10⁶ psi)) fibers, but may also contain discontinuous fiber, fabric, or particulate reinforcement.

1.2 This practice describes established shearography procedures that are currently used by industry and federal agencies that have demonstrated utility in quality assurance of polymer matrix composites, sandwich core materials, and filament-wound pressure vessels during product process design and optimization, manufacturing process control, post manufacture inspection, and in service inspection.

1.3 This practice has utility for testing of polymer matrix composites, sandwich core materials, and filament-wound pressure vessels containing but not limited to bismaleimide, epoxy, phenolic, poly(amideimide), polybenzimidazole, polyester (thermosetting and thermoplastic), poly(ether ether ketone), poly(ether imide), polyimide (thermosetting and thermoplastic), poly(phenylene sulfide), or polysulfone matrices; and alumina, aramid, boron, carbon, glass, quartz, or silicon carbide fibers. Typical as-fabricated geometries include uniaxial, cross ply and angle ply laminates; as well as honeycomb and foam core sandwich materials and structures.

1.4 This practice does not specify accept-reject criteria and is not intended to be used as a means for approving polymer matrix composites, sandwich core materials, or filament-wound pressure vessels for service. (Please note that a flaw does not become a defect until rejected by acceptance/rejection criteria.)

1.5 To ensure proper use of the referenced standards, there are recognized nondestructive testing (NDT) specialists that are certified in accordance with industry and company NDT

specifications. It is recommended that an NDT specialist be a part of any composite component design, quality assurance, in service maintenance, or damage examination activity.

1.6 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.*

2. Referenced Documents

2.1 ASTM Standards:²

C 274 Terminology of Structural Sandwich Constructions

D 3878 Terminology for Composite Materials

D 5687/D 5687M Guide for Preparation of Flat Composite Panels with Processing Guidelines for Specimen Preparation

E 543 Specification for Agencies Performing Nondestructive Testing

E 1309 Guide for Identification of Fiber-Reinforced Polymer-Matrix Composite Materials in Databases

E 1316 Terminology for Nondestructive Examinations

E 1434 Guide for Recording Mechanical Test Data of Fiber-Reinforced Composite Materials in Databases

E 1471 Guide for Identification of Fibers, Fillers, and Core Materials in Computerized Material Property Databases

E 1736 Practice for Acousto-Ultrasonic Assessment of Filament-Wound Pressure Vessels

2.2 Federal Standards:³

21 CFR 1040.10 Laser products

21 CFR 1040.11 Specific purpose laser products

29 CFR 1910.95 Occupational Noise Exposure

2.3 ANSI Standard:⁴

² For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

³ Available from U.S. Government Printing Office Superintendent of Documents, 732 N. Capitol St., NW, Mail Stop: SDE, Washington, DC 20401, <http://www.access.gpo.gov>.

⁴ Available from American National Standards Institute (ANSI), 25 W. 43rd St., 4th Floor, New York, NY 10036, <http://www.ansi.org>.

¹ This practice is under the jurisdiction of ASTM Committee E07 on Nondestructive Testing and is the direct responsibility of Subcommittee E07.10 on Emerging NDT Methods.

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Z136.1-2000 Safe Use of Lasers

2.4 *ASNT Standards*:⁵

SNT-TC-1A Recommended Practice for Personnel Qualification and Certification in Nondestructive Testing

ANSI/ASNT CP-189 Standard for Qualification and Certification of Nondestructive Testing Personnel

2.5 *AIA Document*:⁶

NAS-410 Certification and Qualification of Nondestructive Test Personnel

2.6 *ISO Standard*:⁷

EN 60825-1 Safety of Laser Products - Part 1: Equipment Classification, Requirements, and User's Guide

3. Terminology

3.1 *Definitions*—Definition of terms related to structural sandwich constructions, NDT, and composites appearing in Terminologies **C 274**, **E 1316**, and **D 3878**, respectively, shall apply to the terms used in this practice.

3.2 *Definitions*:

3.2.1 *aerospace*—any component that will be installed on a system that flies.

3.2.2 *beam splitter*—an optical element capable of splitting a single beam of coherent laser light into two beams. Beam splitters are key elements of Michelson Type Image Shearing Interferometers.

3.2.3 *cognizant engineering organization*—see Terminology **E 1316**.

3.2.4 *coherent light source*—a light source that converts electrical energy to a monochromatic beam of light having uniform phase over a minimum specified length known as the coherent length.

3.2.5 *component*—the part(s) or element(s) of a system described, assembled, or processed to the extent specified by the drawing.

3.2.6 *composite material*—see Terminology **D 3878**.

3.2.7 *composite component*—a finished part containing composite material(s) that is in its end use application configuration and which has undergone processing, fabrication, and assembly to the extent specified by the drawing, purchase order, or contract.

3.2.8 *composite shell*—a multilayer filament winding that comprises a second shell that reinforces the inner shell. The composite shell consists of continuous fibers, impregnated with a matrix material, wound around the inner shell, and cured in place. An example is the Kevlar epoxy filament wound spherical shell shown in Figure 1 in Practice **E 1736**. The number of layers, fiber orientation, and composite shell thickness may vary from point to point.

3.2.9 *composite over-wrapped pressure vessel, (COPV)*—see *filament-wound pressure vessel*.

3.2.10 *core crush*—a collapse, distortion, or compression of core material in a sandwich structure.

3.2.11 *core separation*—a partial or complete breaking of honeycomb core node bonds.

3.2.12 *disbond, unbond*—see Terminology **D 3878**.

3.2.13 *de-correlation*—loss of shearography phase data caused by test part deformation exceeding the resolution of the shearing interferometer or motion occurs between the test object and shearing interferometer during data acquisition.

3.2.14 *delamination*—see Terminology **D 3878**.

3.2.15 *displacement derivatives* ($\partial w/\partial x$)—rate of spatial displacement change, where w is the surface displacement and x is the surface coordinates.

3.2.16 *excitation method*—applied stress to a test object used in laser holographic or laser shearographic examination to affect motion at the surface of the test object.

3.2.17 *filament-wound pressure vessel*—an inner shell over wrapped with composite layers that form a composite shell. The inner shell or liner may consist of an impervious metallic or nonmetallic material. The vessel may be cylindrical or spherical and will have at least one penetration with valve attachments for introducing and holding pressurized liquids or gases. Also referred to as a Composite Over-Wrapped Pressure Vessel or COPV.

3.2.18 *flaw, n*—an imperfection or discontinuity that may be detectable by nondestructive testing and is not necessarily rejectable.

3.2.19 *fringe pattern*—a set of lines in a subtraction or wrapped phase shearogram that represents the locus of equal out-of-plane deformation derivative.

3.2.20 *impact damage*—fracturing of epoxy matrix, fiber breakage, inter-laminar delamination of monolithic composites, composite sandwich structure face sheets or filament-wound composite pressure vessels due to impact, characterized by visible dimple surface compression, or fiber breakage caused by impact strike and non-visible subsurface matrix cracking and delamination.

3.2.21 *inclusion*—foreign objects or material including but not limited to particles, chips, backing films, razor blades, or tools of varying sizes which are inadvertently left in a composite lay-up.

3.2.22 *indication*—the observation or evidence of a condition resulting from the shearographic examination that requires interpretation to determine its significance, characterized by dimensions, area, s/n ratio, or other quantitative measurement.

3.2.23 *laser shearography inspection, shearography inspection, shearography*—inspection method utilizing interferometric imaging of deformation derivatives compared between different strain states and designed to reveal non-homogeneities, material changes and structural defects throughout the volume of the material.

3.2.24 *out-of-plane displacement*—the local deformation of a test part, normal to the surface, caused by the application of an engineered force acting on a non-homogeneity or defect in a composite material.

3.2.25 *polymer matrix composite*—any fiber reinforced composite lay-up consisting of laminae (plies) with one or more orientations with respect to some reference direction that are consolidated by press, vacuum bagging, or autoclave to yield an engineered part article or structure.

⁵ Available from American Society for Nondestructive Testing (ASNT), P.O. Box 28518, 1711 Arlington Ln., Columbus, OH 43228-0518, <http://www.asnt.org>.

⁶ Available from Aerospace Industries Association of America, Inc. (AIA), 1000 Wilson Blvd., Suite 1700, Arlington, VA 22209-3928, <http://www.aia-aerospace.org>.

⁷ Available from American National Standards Institute (ANSI), 25 W. 43rd St., 4th Floor, New York, NY 10036, <http://www.ansi.org>.

3.2.26 *porosity*—condition of trapped pockets of air, gas, or void within solid materials, usually expressed as a percentage of the total nonsolid volume (solid + nonsolid) of a unit quantity of material.

3.2.27 *sandwich core material*—an engineered part, article, or structure made up of two or more sheets of composite laminate, metal, or other material designed to support in-plane tensile or compressive loads, separated by and bonded to inner core(s) material(s) designed to support normal compressive and tensile loads such as metal or composite honeycomb, open and closed cell foam, wave formed material, bonded composite tubes, or naturally occurring material such as end grain balsa wood. Also referred to as a structural sandwich construction, see Terminology C 274.

3.2.28 *scan plan*—a designed sequence of steps for positioning and adjusting a shearography camera to accomplish a desired inspection. Scan plans shall include camera field of view, percentage of image overlap, position sequences for each area to be tested, test number, and location in a coordinate system appropriate for test object geometry and access.

3.2.29 *shearogram*—the resulting image from the complex arithmetic combination of interferograms made with an image shearing interferometer and presented for interpretation in various image processing algorithms including wrapped phase maps (static or real-time), unwrapped phase maps, or integrated, Doppler shift map.

3.2.30 *shearography camera, shear camera*—an image shearing interferometer used for shearography nondestructive testing, usually including features for adjustment of focus, iris, zoom, shear vector, and projection and adjustment of coherent light onto the test object area to be inspected.

3.2.31 *shear vector*—the separation vector between two identical images of the target in the output of an image shearing interferometer. The Shear vector is expressed in degrees of angle from the X axis, with a maximum of 90° , with + being in the positive Y direction and – in the negative Y direction. The shear distance between identical points in the two sheared images expressed in inches or millimetres. (See Fig. 1).

3.2.32 *stressing device*—the means to apply a measurable and repeatable engineered stress to the test object during shearography inspection. The applied stress may be in the form of a partial vacuum, pressure, heat, mechanical or acoustic vibration, magnetic field, electric field, microwave, or mechanical load. Also referred to as excitation or excitation method.

3.2.33 *void*—an empty, unoccupied space in laminate. Voids are associated with bridging and resin starved areas.

4. Summary of Practice

4.1 Shearography nondestructive inspection refers to the use of an image shearing interferometer to image local out-of-plane deformation derivatives on the test part surface in response to a change in the applied engineered load. Shearography images tend to show only the local deformation on the target surface due to the presence of a surface or subsurface flaw, delaminations, core damage, or core splice joint separations, as well as impact damage.

4.2 Typical applied loads to the test part are dependant on the test part material reaction to the induced load. The optimum load type and magnitude depend on the flaw type and flaw depth and are best determined before serial testing by making trial measurements. Care is taken to ensure that the magnitude of the applied load is acceptably below the damage threshold of a given test article. The applied load can be any of the following: heat, mechanical vibration, acoustic vibration, pressure and vacuum, electric fields, magnetic fields, microwave, or mechanical load.

4.3 Shearography NDT systems use a common path Michelson, birefringent, or beam splitter type shearing interferometer for imaging defects. Some of the most current technology shearography cameras often use a Michelson type interferometer, Fig. 2, with phase stepping capability. The shearography NDT procedure consists of illuminating a test article with fixed frequency laser light before and after a small proof load is applied. A mirror (the tilt mirror), or other optical device is precisely adjusted to induce an offset, or sheared image, of the

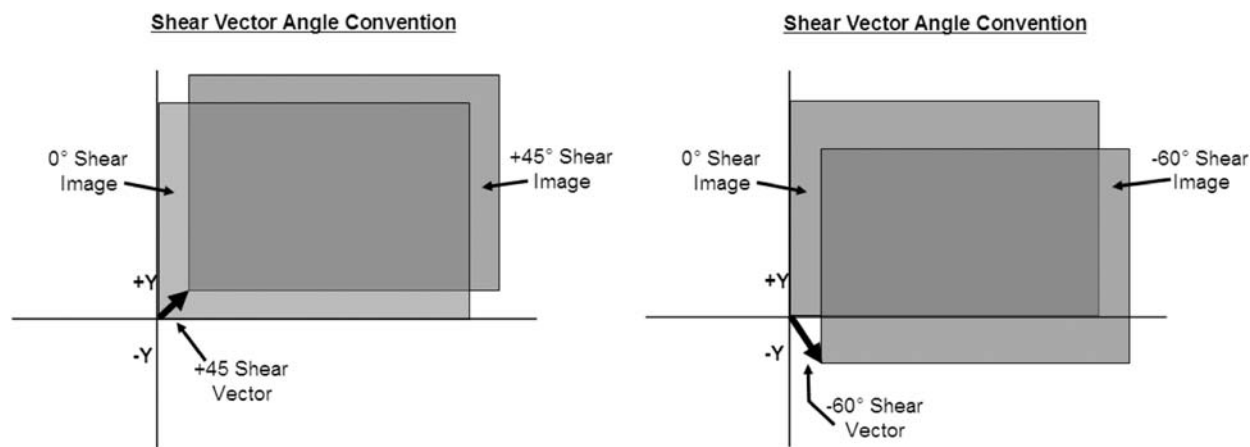


FIG. 1 Shear vector angle convention: Starting with the shear camera adjusted for a 0° shear condition, the sheared image is moved to the right (+ X) or up/down, never adjusted in the direction of $-X$. For a $+45^\circ$ shear vector, the image is moved in the $+X$ and $+Y$ direction. For 60° shear vector, the image is adjusted in the $+X$ and $-Y$ directions. The convention allows determination of deformation direction from the unwrapped phase map.

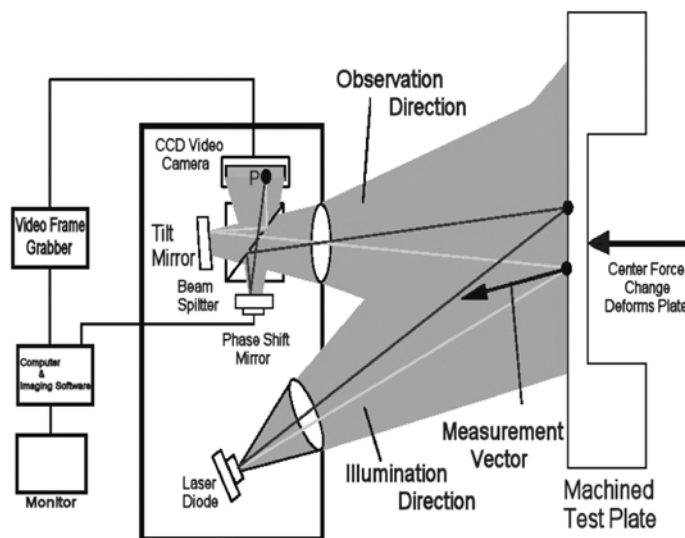


FIG. 2 Schematic diagram of a Michelson type shearing interferometer shown with a shearography calibration device consisting of a metal plate with a machined flat bottomed hole creating a deformable plate with a precision mechanical mechanism for loading at the center point.

test article with respect to a second image of the part. The amount of image shear is a vector quantity with an associated direction, angle, and distance (see Fig. 1). The shear vector, among other factors, determines the sensitivity of the interferometer to surface displacement derivatives, $\partial w / \partial x$. The two sheared images of the test image are focused onto the Charge Coupled Device (CCD) camera. Light from pairs of points in each sheared image interfere with each other, causing interference at every paired point across the field of view. A mirror in the Michelson interferometer may be phase shifted using a piezoelectric device and the sequential interferograms combined to create a phase map of the test object (see Fig. 3) Further processing using any number of unwrapping algorithms may be used to generate fringe free images of local surface deformation derivatives. (see Fig. 4) Each video frame, or interferogram, comprises the complex addition of the two sheared images and can be subtracted from a stored reference image in real time, processed as a dynamic real time phase map



FIG. 3 A phase map shearogram with horizontal shear vector yields a fringe pattern showing the first derivative of the out-of-plane deformation, $\partial w / \partial x$. Using an unwrapping algorithm, the image at right shows the positive (white) and negative (black) slope change.

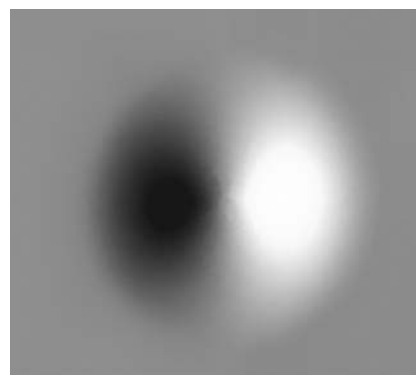


FIG. 4 An unwrapped phase map plots the test part surface deformation derivative without fringes.

or as a static image. Stressed test parts will show out-of-plane deformation (strain concentration) near flaws that is significantly greater than the out-of-plane deformation produced in flaw-free areas. These flaw areas are indicated by the presence of indications in phase maps and unwrapped phase maps. The unwrapped shearography image reveals direction of the test object deforming, either towards or away from the camera. This information may be used to discriminate between repairs, which are stiffer, and damage to aerospace sandwich panels.

4.4 Advantages and Applications—Shearography NDT is full field inspection method and specified area or parts can be inspected in a very short period of time. A sample size of 30.5 cm by 30.5 cm (12 in. by 12 in.) area might take several minutes to set up, then just a few seconds to apply to selected stress technique, collect and processing of the data. Throughputs range from 4.6 to 46 m²/h-1 (50 to 500 ft²/h-1) depending on the degree of automation, compared to 0.93 m²/h-1 (10 ft²/h-1) throughput typical of Ultrasonic Testing (UT) C-Scan, depending on scan increment step size. Shearography inspection is non-contact, non-contaminating and does not require couplant or submersion. For production systems, shearography

camera is typically located from 0.6 to 1.8 m (2 to 6 ft) from inspection area and will not contact the inspection part. However, the applied loading method may require contact such as a vacuum window placed on the part or a transducer designed to vacuum attach to vehicle surfaces in some applications for a mechanical stress of the part. Portable shearography systems for on-vehicle inspection are designed to vacuum attach to vehicle surfaces. Care must be taken to ensure no damage to very thin composite face sheets will be caused by such contact.

4.4.1 Inspection results can be kept as a permanent record and available for future evaluation and presentation. With some software the data can be stored as a JPG, TIF, or other image format. The raw data is stored and can be processed and evaluated at any time. Shearography systems utilize tools such as video calipers to allow for rapid defect sizing and area measurement.

4.4.2 Shearography has been used with excellent results for filament-wound pressure vessels, composite and metal face sheet sandwich panels with both honeycomb and foam cores, solid monolithic composite laminates, foam cryogenic fuel tank insulation, bonded cork insulation, aircraft tires, and elastomeric and plastic coatings. Frequently, defects at multiple and far side bond lines can be detected.

4.5 *Limitations and Interferences*—The laser light used in shearography inspection is not a penetrating radiation. Shearography images subsurface flaws indirectly cause surface deformations above the flaw, in the range from 1 nm to 500 microns, which are detected by the shearography camera. These deformations are detected by the shearography camera. Shearography therefore is less sensitive to defects as the defect depth increases. Shearography is applicable to non-brittle materials, where critical flaw size is smaller than the detectable limit. Shearography may not be applicable to materials with very high rigid strength, low or negative coefficient of thermal expansion, or thick face sheet thicknesses.

4.5.1 *Ambient light*—Ambient light may overpower the low laser power density diffusely reflected from the test part, degrading the shearography data. Most portable equipment includes features to allow testing in full daylight. Production shearography systems operate in test cells or away from high intensity ambient lighting.

4.5.2 *Test part color and reflectivity*—Shearography requires imaging diffuse laser light reflected from the test part surface to create a full field image. The optimal surface is flat white. The worst condition for shearography inspection is a spherical or convoluted, gloss black test part. The glare from a spherical or convoluted surface and the specular reflection from the gloss surface create an extreme intensity distribution that degrades the shearography data. In these worst cases, coatings such as dye-penetrant developer may be applied to reduce glare and increase reflectivity.

4.5.3 *Ambient vibration or test part motion*—Ambient vibration or motion can degrade shearography image quality or prevent any useful image from being obtained. Usually vibration or part motion is predominately in one direction. Rotating the shear vector can reduce sensitivity in the direction motion

is most prominent. Shimming the test piece and checking for part or camera movement can help eliminate the detrimental effects of motion.

5. Significance and Use

5.1 Shearography is commonly used during product process design and optimization, process control, post manufacture inspection, and in service inspection, and can be used to measure static and dynamic axial (tensile and compressive) strain, as well as shearing, Poisson, bending, and torsional strains. The general types of defects detected by shearography include delamination, deformation under load, disbond/unbond, microcracks, and thickness variation.

5.2 Factors that influence shearography and therefore shall be reported include but are not limited to the following: laminate (matrix and fiber) material, lay-up geometry, fiber volume fraction (flat panels); facing material, core material, facing stack sequence, core geometry (cell size); core density, facing void content, and facing volume percent reinforcement (sandwich core materials); processing and fabrication methods, overall thickness, specimen alignment, specimen conditioning, specimen geometry, and test environment (flat panels and sandwich core materials).

6. Equipment and Materials

6.1 The general shearography apparatus is shown schematically in Fig. 2, and shall include the following:

6.1.1 *Laser shearography camera*—The shearography camera shall have demonstrated the ability to detect the maximum allowable defect size and depth in similar material and structure as will be inspected and sufficient laser power to illuminate the test part. Shear cameras are available with either fixed or adjustable shear vector.

6.1.2 *Camera control and calibration device*—This device consist of controls to manipulate the camera and laser during the evaluation process. The first control allows for camera motion in the vertical (tilt) and horizontal (pan) planes. The second control permits adjustment of the cameras aperture size. The third control operates the cameras zoom lens focal length and its focus. A separate control operates the tilt adjustment of the shearing mirrors within the camera to enable the ability to shear the image both horizontally and vertically independent of one another. The shearography laser controls allow the laser to be rotated in the vertical plane (tilt) and in the horizontal plane (pan) with an expansion adjustment to disperse the laser as needed.

6.1.3 *Image capture and processing computer*—The computer must be capable of capturing and saving images when instructed. The computer must then have the ability of converting the images to a digital format to allow for multiple signal processing techniques to be applied. These techniques vary with each individual application. The computer should have the ability to place adjacent consecutive images next to one another to allow for a full field view of the inspected component.

6.1.4 Stressing device—The stressing device shall be capable of introducing a loading into the article to be evaluated. This loading shall be capable of producing small nondestructive deformations on the part or component, which will produce stress within the article.

6.1.4.1 Vacuum stressing—This type of stressing system consists of a sealed vacuum chamber, air movement device such as a blower, and vacuum relief valves located between the chamber and atmospheric pressure. The blower displaces air thereby decreasing the pressure within the chamber. The decrease differential required to stress the tested article is typically in the 0.7 to 14.0 kPa (0.1 to 2.0 psi) range. The vacuum relief valve is used to bring the pressure between the chamber and atmosphere to steady state.

6.1.4.2 Thermal stressing—Any device that can introduce heat into the area of the article being evaluated may be used to increase test piece surface temperature. High intensity quartz lamps, and standard heat guns are commonly used. Manufactured thermal stressing devices with temperature measurement feedback are also used to provide a rapid, uniform temperature increase across the field of view on the test part.

6.1.4.3 Pressure stressing—This system consists of a source of compressed gas meeting cleanliness requirements for the test pressure vessel, associated valves and plumbing that are used to pressurize filament-wound pressure vessels. During inspection the vessels are brought up to a bias pressure greater than atmospheric pressure. This bias pressure is used as a baseline for testing. The pressure is then cycled between a pressure either greater than or less than the bias pressure. The amount of pressure differential is a function of the tank material, and geometry. The shearography data taken with increasing pressure will have a reverse phase compared to data taken with decreasing pressure.

6.1.4.4 Acoustic Vibration Stressing—The device must be capable of introducing small time dependant oscillations into the test article. This is commonly done using an air coupled acoustic device, which consists of a signal generator, a signal amplifier and an acoustic driver. The acoustic driver converts electrical energy to a highly focused acoustic pressure wave that travels through the air from the driver to the article being evaluated. The acoustic driver is strategically placed at a distance and angle to the evaluated article to optimize the ratio of longitudinal and shear waves entering the article.

6.1.4.5 Mechanical Vibration Stressing—A mechanically or vacuum attached piezoelectric actuator is an alternative vibration stressing device. This device consists of a signal generator, an actuator drive, and a linear mechanical actuator. The piezoelectric actuator is coupled rigidly to the component being tested. A sinusoidal signal or other waveform is then sent to the actuator causing a desired vibration and amplitude. This vibration is then transmitted through the test article.

6.1.5 Test Specimen Fixture Apparatus—The apparatus must perform the function of minimizing any movement that is not relative between the shearography camera and the article being evaluated. This type of unwanted movement will result in shearography image decorrelation.

6.1.5.1 Polymer Matrix composite and sandwich core material fixture—The fixture consists of a device capable of rigidly supporting the monolithic or sandwich core material to minimize movement.

6.1.5.2 Filament-wound pressure vessel fixture—The fixture consists of a device capable of rigidly supporting a pressure vessel to minimize uniform global movement/vibration caused by vessel pressurization. The apparatus should also allow the pressure vessel to rotate about an axis enabling the shearography scan plan to be executed. The fixture should have a degree plate on each axis to allow accurate rotation of the vessel and naming each shearography of file with the location angle. Finally, a pressure gauge mounted to provide the shearography Operator with the instantaneous tank pressure is required, to allow shearography data capture at the correct pressure. Automated pressurization systems, with calibrated pressure sensors and gas flow valves controlled by the shearography computer, are also in use.

6.2 Equipment calibration—Each shearography instrument or system, when calibration is required, shall have either a calibration sticker affixed, or record of certification on file, containing the following:

6.2.1 Instrument calibration.

6.2.2 Serial number.

6.2.3 Calibration date.

6.2.4 Calibration due date.

6.2.5 Name of individual who performed last calibration.

6.2.6 If calibration is not required, a sticker, stating no calibration is necessary shall be affixed, or a record shall be on file to this effect.

6.2.7 Shearography instruments and systems shall be calibrated against currently-certified standards calibrated by accepted government or industrial agencies (or shall indicate that it is calibrated as used, or that no calibration is necessary) at periodic intervals where specified.

6.3 Facility qualification—If specified in the contractual agreement, NDE facilities shall be qualified and evaluated in accordance with Practice E 543. The applicable revision of Practice E 543 shall be specified in the contractual agreement.

6.4 Personnel Qualification—If specified in the contractual agreement, personnel performing NDE tests shall be qualified in accordance with a nationally recognized NDE personnel qualification practice or standard such as ANSI/ASNT CP-189, SNT-TC-1A, NAS-410, or similar document and certified by the employer or certifying agency as applicable. The practice or standard used and its applicable revision shall be identified in the contractual agreement between the using parties. For example, the levels of qualification per NAS-410 are Trainee, Level 1 “Limited”, Level 1, Level 2, Level 3, Instructor, and Auditor.

6.5 Materials:

6.5.1 Polymer matrix composite specimens—processing guidelines that facilitate fabrication of monolithic composite specimens made from unidirectional tape or using orthogonal weave patterns are found in Guide D 5687/D 5687M. For specimen preparation using other processing techniques, for

example, pultrusion, filament winding, and resin transfer molding, processing guidelines are not available and shall be agreed upon by the using parties.

6.5.2 *Sandwich core specimens*—processing guidelines for fabrication of sandwich construction specimens are not available at this time, and shall be agreed upon by the using parties.

6.5.3 *Filament-wound pressure vessel specimens*—processing guidelines for specimen preparation using filament winding are not available at this time, and shall be agreed upon by the using parties.

7. Procedure

7.1 *General Shearography Procedure*—Select the optimal stressing technique for the desired application. Place the article to be evaluated in a secure, rigid fixture to minimize undesired movement that may be produced during testing. Place the laser shearography camera at a distance from the part where an optimal field of view can be obtained. The field of view on some cameras can be adjusted using the zoom feature on the camera controller. The focus of the camera is now to be set using the focus feature on the camera or controller. The optimal focus setting is achieved when image distinctness or clarity is at its best. Depending on the material, the camera view may be adjusted slightly off the orthogonal view to minimize direct laser reflection that may cause light saturation on the shearographic image. This can be accomplished by using either the “tilt” or “pan” adjustment on the camera controller. The system then must be calibrated to assure accuracy. This process is completed by placing a system of two points whose distance between one another is known in the field of view on the test specimen. The shear vectors, horizontal, vertical, or both can be adjusted at this point depending on the application. This is accomplished by using the shear controls on the camera controller. A straightedge held to the surface of the inspection part works well to quantify the value. The chosen stressing technique is now applied to the part; a reference shearography image is taken prior to stressing the part, then a stressed shearography image is taken. The images are then combined for a phase map shearogram that may be further image processed. (See Table 1.)

7.2 *Thermal Shearography Procedure*—Thermal shearography images changes locally in the coefficient of thermal expansion. Thermal shearography can be applied in two ways.

7.2.1 *Procedure 1*—Capture the reference Image P1, apply heat to area, wait time T for thermal diffusion to take place, capture final image P2 and process.

7.2.2 *Procedure 2*—Heat first, capture reference image P1, wait time “T” for thermal diffusion, capture final image P2, and process. The amount of heat needed to stress the area to be inspected is a function of the material thermal properties and the thickness of the material to be inspected. Repeatability requires precision timing of all parameters. Fig. 5 shows a sample result shearography image.

7.3 *Pressure Shearography Procedure*—Typically used for pressure vessels, vented core honeycomb panels, and rocket engine combustion chamber hot walls. A pressure vessel is brought to a steady state bias pressure or approximately 0.1 to 1.0 % of the working pressure. The shearography reference image P1 of the area to be inspected is then captured. From this point, the pressure can be either increased or reduced by approximately 0.5 % of the working pressure, or until the limit before the image decorrelates as determined by experiment. Fig. 6 shows a sample result shearography image.

7.4 *Vacuum Shearography Procedure*—The article to be evaluated is placed in a shearography vacuum test chamber. A shearography reference image, P1, is captured of the area to be inspected, air is then expelled from the chamber creating a partial vacuum, typically 9.4 kPa (1.4 psi) below ambient pressure within the chamber. Contained air, still at ambient pressure within the core material exerts an out-of-plane force on the sandwich panel face sheet at the site of the defect A stressed shearography image, P2, is then captured and the image processed. The chamber is vented to the atmosphere, the camera moves to the next area on the part for inspection. This process can be reversed by first collecting the reference stressed image during the reduced pressure state and the unstressed image collected at atmospheric pressure. Portable Vacuum Shearography systems that vacuum attach in place onto the vehicle structure operate the same way. Fig. 7 is a sample result shearography image.

TABLE 1 Shearography Procedure by Material, Structure and Defect Type

NDT Method	Material				
	Monolithic Laminate	Composite Honeycomb	Metal Honeycomb	Coatings, Foam, Cork, Rubber	COPV
Thermal Shearography	- Impact Damage - Delamination - Porosity	- Impact Damage - Delamination - Disbonds	- Disbonds - Crushed Core - Insert Location	NA	NA
Pressure Shearography	NA	Vented Core: - Impact Damage - Disbonds	Vented Core: - Impact Damage - Disbonds	NA	- Impact Damage - Delamination - Bridging - Manufactured Flaws
Partial Vacuum Shearography	NA	- Disbonds - Crushed Core - Insert Location - Far Side Disbonds	- Disbonds - Crushed Core - Core Splice Disbonds - Far Side Disbonds	- Disbonds - Voids - Damage	Liner Disbonds
Vibration Shearography	- Impact Damage - Delamination - Disbonds	Perforated Skins: - Disbonds - Crushed Core	Perforated Skins: - Disbonds - Crushed Core	NA	NA

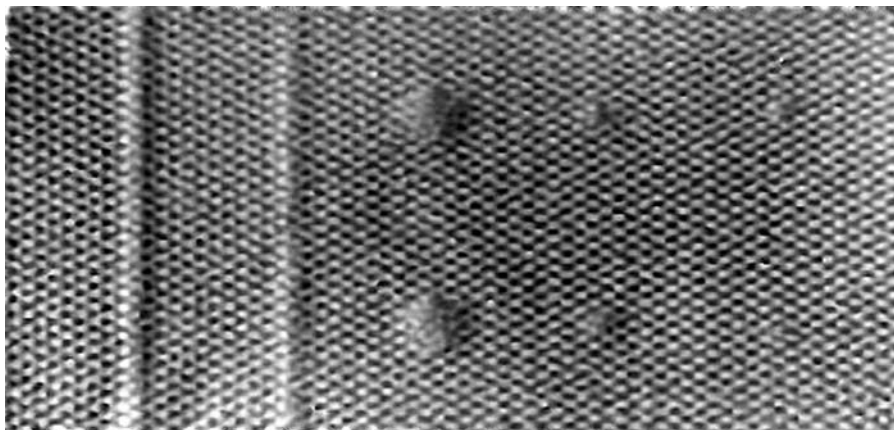


FIG. 5 Thermal shearography of a 25.4 by 12.7 cm (10 by 5 in.) aluminum honeycomb panel with graphite face sheets. Test panel surface temperature was raised 5°F, P1 captured, wait time was T=5 seconds then P2 was captured. The phase map was unwrapped and non-linear trend removal applied. All near and far side defects are detected.

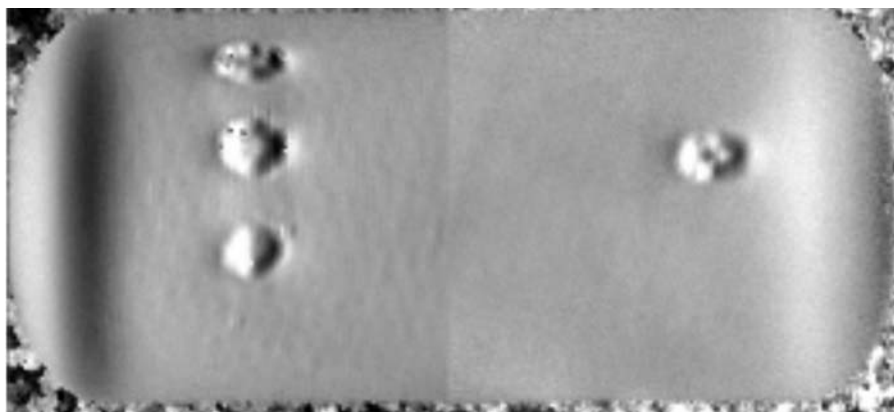


FIG. 6 Graphite filament-wound pressure vessel, or COPV, tested with shearography using only 14 kPa (2.0 psi) pressure change to image non-visible subsurface damage to the composite material. Operating pressure of this COPV is approximately 41.4 MPa (6000 psi).

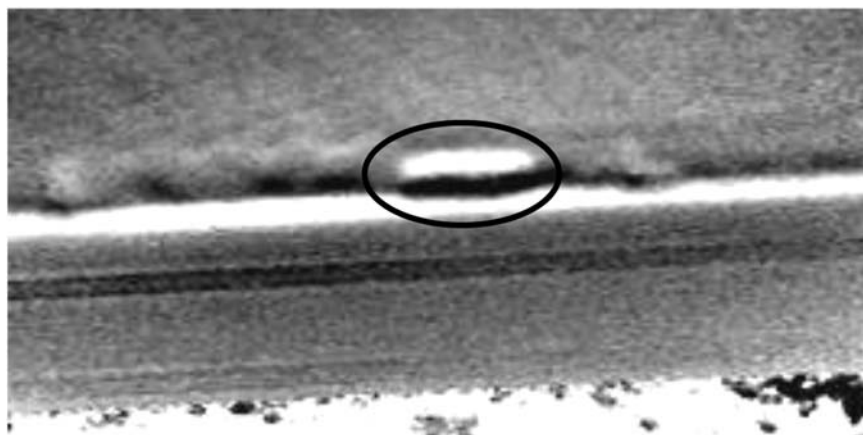


FIG. 7 Typical graphite face sheet to Nomex honeycomb disbond shown inside circle. Disbond measures 1.45 by 0.35 inches.

7.5 Vibration Shearography Procedure—Dynamic stressing techniques use mechanically or vacuum attached (MECAD) or air-coupled vibration excitation (ACAD) and employ Phase Reversal Shearography. The image of the defect appears

continuously in real-time (see Fig. 8) or may be captured as a static image. The operator applies the excitation and captures

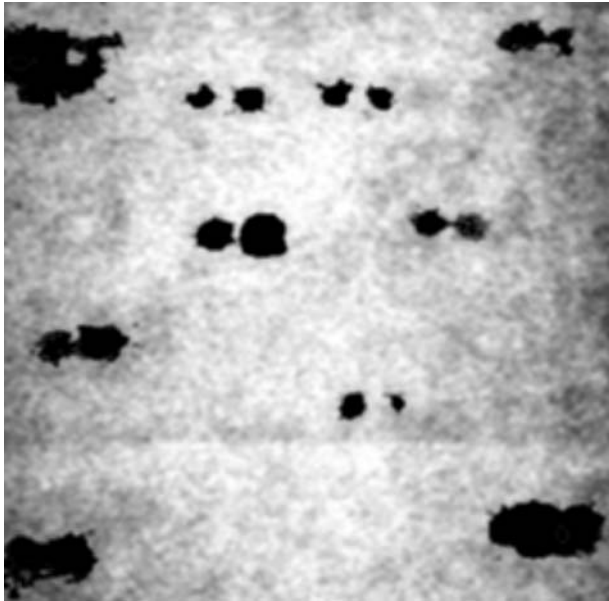


FIG. 8 Acoustic shearogram of rocket fuel tank spray on foam insulation showing detected voids between the substrate and the foam. Field of view is 20 by 20 in. and the test time was 0.5 seconds.

the image of the defect. MECAD exciters are piezoelectric devices with vacuum attachment or mechanical attachment features.

7.6 Acoustic Vibration Shearography—Provides totally non-contact, remote inspection capability for light weight, composite honeycomb structures and foam type thermal protection materials used for launch vehicles.

8. Safety and Hazards

8.1 Laser Safety—Shearography uses laser light to illuminate the surface of the test article under inspection. A laser is simply a convenient source of monochromatic and coherent light that makes the implementation of shearography possible. With the exception of extremely low powered laser systems, virtually all laser products pose some form of hazard; most often associated with the direct exposure of the eyes and skin to the laser light. Laser systems are classified in the United States in accordance with the Center for Devices and Radiological Health (CDRH) division of the Food and Drug Administration (FDA). The applicable federal documents are **21 CFR 1040.10** and **21 CFR 1040.11**. In the European community, laser system standards are overseen primarily by the International Electrotechnical Commission (IEC) and the British Standards Institution (BSI). The applicable European document is **EN 60825-1**. Additional federal, state, and local regulations may also apply to the use and classification of laser products depending on the intended location of the system. Many of these regulations are based on classification data provided by the American National Standards Institute (ANSI). **ANSI Z136.1-2000** provides detailed information regarding hazard evaluation and classification, control measures, laser safety programs and employee training, medical surveillance, non-beam hazards, criteria for exposure of eye and skin, and small and extended source measurements. From a practical

standpoint, laser shearography systems should be classified so as to provide the most usable system for the operator with the least restrictions. To minimize hazard and restrictions, systems with classification of Class 1, 2, and 3a (3r IEC) are the preferred classifications for shearography systems.

8.1.1 Systems classified as Class 1 and 2 laser systems generally do not require any special safety consideration beyond a basic understanding of the safe use of lasers. Under normal working conditions, Class 3a laser systems extend allowable output emissions of the laser system by five times those of Class 2 laser systems without adding additional restrictions beyond a more in depth knowledge of safe laser operation. When using Class 3a laser systems, care must be taken not to view the laser emissions with any optical system that will increase concentration of the laser light (that is, binoculars or telescopes). This does not include normal corrective lenses.

8.1.2 Class 3b and Class 4 laser systems should generally be avoided for all but laboratory systems due to required operating restrictions and the need for additional medical surveillance.

8.2 Acoustic Noise Hazards—Hazardous levels of acoustic noise are not generally directly associated with the application of shearography nondestructive testing but may be a by-product of the stressing methods being employed during its application. A principle example of this is the use of acoustic or mechanical vibration stressing. In the case of acoustic stressing, large speakers are used to vibrate the test article under examination. Sound pressures levels associated with this form of stressing may exceed 130 dB when approaching the source of acoustic emissions.

8.2.1 Within the United States, noise exposure regulations for general industry are defined by Occupation Safety and Health Administration (OSHA) as documented within **29 CFR 1910.95**. In accordance with **29 CFR 1910.95**, noise exposure to sound levels above 85 dB must be regulated through either environmental controls or the use of personnel protective devices such as “ear plugs” or “muffs”. Long term exposure to sound levels above 85 dB has been shown to produce gradual hearing loss in many individuals.

8.2.2 Sound pressure levels referenced by this practice can be readily measured using inexpensive sound level meters available through many audio and electronic supply houses. The measurements are made using an “A-weighted” – “slow response” setting. Limitations as to the permissible time over which an individual can be exposed to increasing levels of noise are defined within Table G-16 of standard **29 CFR 1910.95** and range from 8 h at 90 dBA to 15 min at 115 dBA. Additionally, no exposure to sound intensities greater than 140 db must be permitted. (Be especially careful of high intensity sound impulses that may be generated during the impacting of composite samples during the creation of test standards.)

8.2.3 Due to variations in the application of acoustic stressing, a worse case exposure corresponding to the maximum output of the acoustic driver over the expected work period (up to 8 h/day) should be assumed. Noise protection devices should be selected such as to bring personnel exposure levels to no more than 90 dB over the course of an eight hour work day (preferably 85 dB).

8.2.4 General noise recommendations for acoustic and mechanical vibration stressing:

8.2.4.1 Always use the minimum required for the inspection being performed.

8.2.4.2 Always assume that the noise source is potentially active unless it has been rendered safe (preferably by means of removal of power).

8.2.4.3 Be conscious of both operator and bystander exposure levels. If personnel other than those performing an inspection are present, ear protection should be made available to them.

8.2.4.4 Post warning signs outside the “danger area” to warn individual entering the test area of possible high intensity noise exposure.

9. Precision and Bias

9.1 Shearography is suitable for making quantitative measurements of anomaly characteristics that include x and y dimensions, the z axis deformation in response to an applied load change, and in certain cases, depth. The magnitude and nature of the error in shearography-based measurements depends of the particulars of the shearographic equipment, data acquisition parameters, the test article (specimen), and the nature of the defect (for example, delamination, deformation under load, disband/unbond, microcracks, thickness variation).

9.2 Quantitative shearography requires precision calibration of the image scale in pixels/mm (pixels/in.), and shear vector. A shearography calibration device (see Fig. 9), shall be used to verify shearography equipment calibration. The use of such quantitative measurements requires that the errors associated with them be established.



FIG. 9 A shearography camera calibration device consists of a means to apply a known deformation to an aluminum flat plate. The flat surface deformation is imaged. This device allows verification of the shearography camera operation, laser stability, and the minimum coherence length.

9.3 *Precision*—The precision of the measurements can best be measured by seeing the distribution of measurements of same feature under repeated scans, preferably with as much displacement or deformation in the specimen as in practice or as required for a Probability of Detection Analysis. This ensures that all effects which vary results are allowed for, such as alignment artifacts, drift, and camera to target surface angle.

9.4 *Bias*—In addition to random variation, measurements of any feature may also have consistent bias. This may be due to artifacts in the shearogram, or to false assumptions used in the measurement algorithm.

9.5 Examination of the distribution of measurements results from repeated scans of test objects with known features similar to those which are the target of the NDT investigation, is the best method for determining precision and bias in shearography. Once such determinations have been made for a given system and set of test articles and data acquisition conditions, they can be used to give well based estimates of precision and bias for other test articles of similar size, composition, and form, as long as no unusual artifact patterns are introduced into the shearograms.

9.6 To ensure material traceability, essential information about the composite material, reinforcement, matrix, preform, prepreg, process method, and part information shall be recorded as described in Guide E 1309. Additional information may be necessary when individual constituents that make up the composite material being tested are considered independently. For example, for identification of reinforcements in terms of class, subclass, chemical family, form, dimensional parameters, and dimensional distribution Guide E 1471 should be consulted.

9.7 To ensure test validity, including reproducibility and repeatability, essential information about test method, specimen preparation, specimen geometry, specimen conditioning, test equipment, transducer (if applicable), test environment, loading (if applicable), raw and normalized data, and statistical analysis (if applicable) shall be recorded as described in Guide E 1434.

10. Keywords

10.1 aerospace composites; composites; COPV; fiber-reinforced polymer matrix composites; filament-wound pressure vessels; high modulus fibers; high performance composites; honeycomb core; laminates; nondestructive evaluation (NDE); nondestructive inspection (NDI); nondestructive testing (NDT); polymer matrix composites (PMC); sandwich constructions; sandwich core materials; shearography; structural sandwich constructions; thermal shearography; vacuum stress shearography; vibration stress shearography

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